

LO of the frequency downconverter for the received signal. An IF is introduced by offsetting the latter using another upconverter and a low frequency oscillator. This oscillator is also used for providing the LO of the final I/Q demodulator converting the IF signal to baseband. Reducing the number of K_a -band oscillators will have a positive impact on the reliability of the system, as these devices have proved to be a source of unreliability with the three systems produced to date.

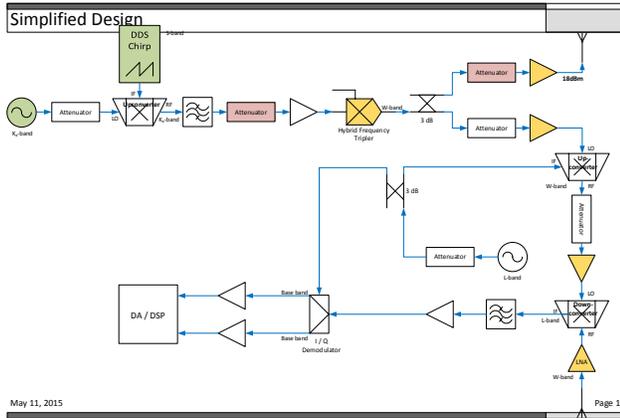


Figure 2: Example for a potential re-design of the RAL Radar Cloud Profiler RF frontend. Components marked yellow are based on in-house development or capabilities.

In-house capabilities (e.g. bonding, packaging, component design) and developments will be utilised for providing driver and power amplifiers at W-band. Furthermore, a hybrid (as opposed to purely active or passive) frequency tripler based on biased Schottky diodes [9] will be applied. Another component developed in-house that potentially could be utilised and allow further extending the fraction of the signal handled at K_a -band would be a 3rd harmonics mixer.

3. REALISATION

The re-design will be realised in three phases. The first phase will be setting up a breadboard demonstrator as displayed in Figure 3. This will omit the step introducing an IF, but will allow assessing the components intended for use in the final design under realistic conditions. It also will allow testing the data acquisition / digital signal processing system and demonstrating the Doppler capability. Results from this phase will be presented.

The second phase will be to set up the system according to Figure 2 on a breadboard taking into account the findings from Phase 1.

The third phase will be the assembly of the final re-design in a weatherproof housing. This will be assessed in routine operation at RAL and deployed for atmospheric research campaigns.

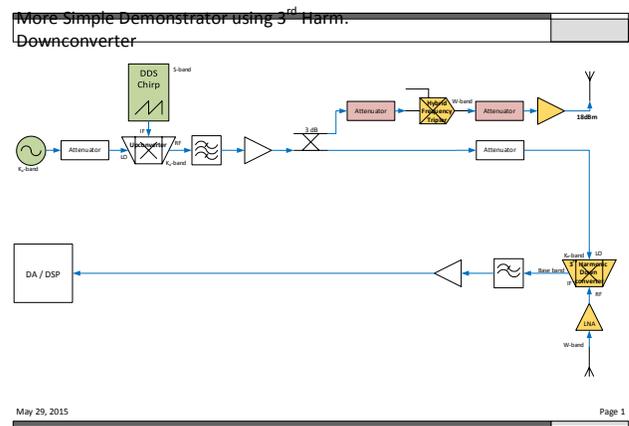


Figure 3: Breadboard demonstrator for the re-design of the RAL Radar Cloud Profiler RF frontend. Components marked yellow are based on in-house development or capabilities.

At this point in time, the assessment of further options is still a possibility. These could involve further system simplification, e.g. using the DDS chirp instead of an additional oscillator for generating the IF as detailed in Figure 2. Options also could arise from further in-house component development.

4. RESULTS

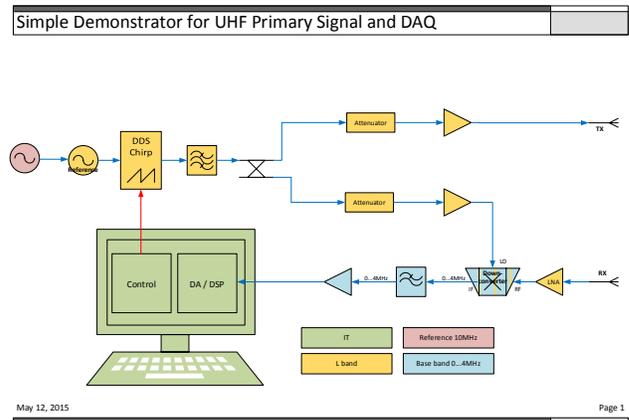


Figure 4: Simple demonstrator for primary signal generation in L band and for testing data acquisition system.

First activities in the project have focused on setting up a demonstrator for generating the primary signal. The concept for this is shown in Figure 4. The demonstrator also serves the purpose of testing the data acquisition (DA) system. This demonstrator already utilises the Direct Digitisation Source (DDS) that is planned to be used in the RF design for the complete system. This is supplied with a fixed-frequency reference signal by a phase-locked coaxial resonator oscillator (PCRO), which in return is provided

with a 10 MHz reference signal by an oven-controlled crystal oscillator (OCO).

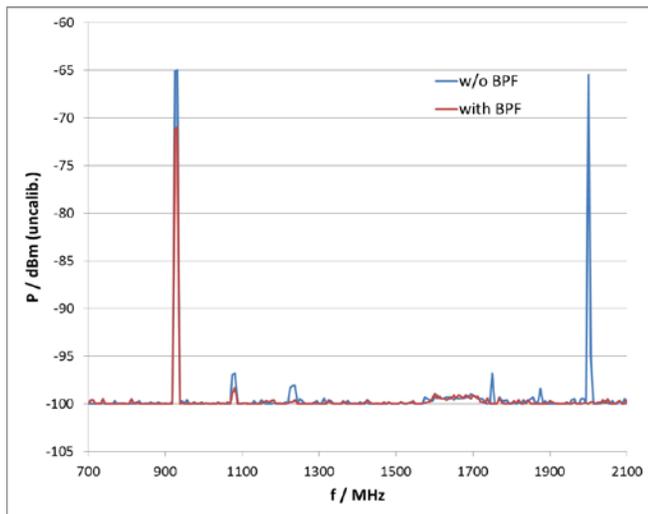


Figure 5: Output of the DDS for a 5 MHz chirp on top of a carrier frequency of 921.5 MHz. The blue line indicates the signal as generated from the DDS. The red line shows the signal after applying a band pass filter with a pass band of 145...1000 MHz.

The DA system applied in the demonstrator will most likely be upgraded for the future complete system. However, the basic signal processing and retrieval algorithms will remain the same. It also should be noted that signals arriving at the DA part of the future complete system will be in the same frequency range – base band 0...4 MHz.

The first step in setting up the demonstrator was to assess the DDS used for generating the primary signal at L band. An example for a 5 MHz chirp on top of a carrier frequency of 921.5 MHz can be found in Figure 5. The blue line in this figure indicates the signal as generated by the DDS. This shows a strong undesired signal at the reference frequency of the DDS (2000 MHz), and some other spurious signals. Applying a band pass filter with a pass band of 145...1000 MHz eliminated the signal at the reference frequency and got rid of most of the other spurious signals. This is indicated by the red line in Figure 5.

5. OUTLOOK

Following the finalisation of the demonstrator for generating the primary signal at L-band as shown in Figure 4, the DA system will be set up and tested. This combination will be thoroughly assessed in the laboratory. There might also be the opportunity to test it with real atmospheric observations during rainfall.

These subsystems will be used further for setting up the simple demonstrator at W-band according to Figure 3. This demonstrator again will be thoroughly tested in the

laboratory. Furthermore, the opportunity for testing it with real atmospheric observations during rainfall and fog periods might arise.

Eventually the re-designed W-band Doppler radar cloud profiler as shown in Figure 2 will be built. After thorough tests in the laboratory, this system shall be deployed for atmospheric observations at the Earth and Atmospheric Observations Group at RAL. It is anticipated that the system also will be employed for field campaigns and demonstrations in collaborations with universities, research institutes and national weather services.

6. REFERENCES

- [1] Sauvageot, H. [Radar Meteorology], Artech House Publishers (1992).
- [2] Lhermitte, R., "A 94 GHz Doppler Radar for Cloud Observations", J. Atmos. Oceanic Tech. 4, pp 36-48 (1987).
- [3] Illingworth, A. J., Hogan, R. J., O'Connor, et al., "Cloudnet – continuous evaluation of cloud profiles in seven operational models using ground-based observations", Bull. Am. Meteorol. Soc. 88, pp 883-898 (2007).
- [4] Lyth, D., Nash, J. and Oldfield, M. "Observing fog and low cloud with a combination of 78 GHz cloud radar and laser ceilometer", Proc. WMO Tech. Conf. Meteorological & Environ. Inst Methods of Observation, P2(11) (2005).
- [5] Bennett, A. J., Gaffard, C., Oakley T., Oldfield, M. L., Huggard, P. G. and Moyna B. P., "Cloud radar – initial measurements from the 94 GHz FMCW radar", Proc. WMO Tech. Conf. Meteorological & Environ. Inst Methods of Observation (TECO-2008).
- [6] Maier, F., Bendix, J., and Thies, B., "Simulating Z-LWC Relations in Natural Fogs with Radiative Transfer Calculations for Future Application to a Cloud Radar Profiler", PURE AND APPLIED GEOPHYSICS 169(5-6), pp. 793-807 (2012).
- [7] Neil I. Fox and Anthony J. Illingworth, "The Retrieval of Stratocumulus Cloud Properties by Ground-Based Cloud Radar", JOURNAL OF APPLIED METEOROLOGY 36(6), pp. 676-687 (1997)
- [8] Ewan J. O'Connor, Robin J. Hogan, and Anthony J. Illingworth, "Retrieving stratocumulus drizzle parameters using Doppler radar and lidar", JOURNAL OF APPLIED METEOROLOGY, 44(1), pp. 14-27 (2005).
- [9] Hui Wang, Byron Alderman, Simon Rea, Hoshiar Sanghera, Mark Merritt, N. J. Brewster and P. G. Huggard, "Full W-band discrete Schottky diode frequency tripler with integrated on-chip capacitor", STFC / RAL internal communication (2014).