

# Impedance of Ultrarelativistic Charged Distributions in Tapering Geometries

D.A. Burton, D.C. Christie, R.W. Tucker, Lancaster University and The Cockcroft Institute, UK

## Abstract

We develop a scheme for obtaining the impedance of a gradually tapered, axisymmetric geometry containing a bunch of arbitrary profile travelling at the speed of light parallel to the axis of the taper. Coordinate-free expressions for Maxwell's equations are 2+2-split in a coordinate system adapted to the particle beam and the taper and, using an asymptotic expansion for a gradual taper, a coupled hierarchy of Poisson equations is obtained. Applications of the scheme are presented.

## INTRODUCTION

The design of accelerator components such as collimators relies on understanding the consequences of passing an ultrarelativistic charged beam through a waveguide with a gradual taper. This is currently studied using a combination of experiment and computer simulation. However, various analytical methods have also been developed to estimate impedances (see, for example, [1]). Most recently, Stupakov [2] developed a process for evaluating the impedance up to the second order of iteration for low frequency beams travelling at  $v = c$  in perfectly conducting waveguides of arbitrary cross-section. We shall use a similar method, restricted to axially symmetric confining geometries [3]. However, our approach, using auxiliary potentials, enables us to relax Stupakov's low-frequency condition and produce a hierarchy of equations that can be solved to arbitrary order.

## MAXWELL EQUATIONS AND BOUNDARY CONDITIONS

The spacetime metric  $g$  is given in cylindrical polar coordinates by<sup>1</sup>

$$g = -dt \otimes dt + dz \otimes dz + dr \otimes dr + r^2 d\theta \otimes d\theta \quad (1)$$

and the transverse, cross-sectional domain  $\mathcal{D}$  at fixed  $t$  and  $z$  has the induced metric

$$g_{\perp} = dr \otimes dr + r^2 d\theta \otimes d\theta \quad (2)$$

In spacetime, the Hodge map and exterior derivative are denoted  $\star$  and  $d$ , and in the transverse domain, they are denoted by  $\#_{\perp}$  and  $d_{\perp}$ . The transverse co-derivative  $\delta_{\perp}$  is defined as

$$\delta_{\perp} = \#_{\perp}^{-1} d_{\perp} \#_{\perp} \eta \quad (3)$$

<sup>1</sup>We work in the MKS system, with units in which the speed of light  $c = 1$ .

where  $\eta\omega = (-1)^p\omega$  for any  $p$ -form  $\omega$  and  $\#_{\perp}1 = r dr \wedge d\theta$ .

The source, moving in the positive  $z$ -direction at the speed of light, has charge density  $\rho$  and 4-velocity field

$$V = \partial_t + \partial_z \quad (4)$$

The vacuum Maxwell equations for the spacetime 2-form  $F$  are given by

$$dF = 0, \quad d \star F = -\frac{\rho}{\epsilon_0} \star \tilde{V} \quad (5)$$

where  $\tilde{V} = g(V, -)$  and  $\epsilon_0$  is the permittivity of free space. In terms of new co-ordinates

$$u := z - t, \quad \zeta := z \quad (6)$$

the metric and volume 4-form  $\star 1 = dt \wedge dz \wedge \#_{\perp}1$  become

$$g = d\zeta \otimes du + du \otimes d\zeta - du \otimes du + g_{\perp} \quad (7)$$

$$\star 1 = d\zeta \wedge du \wedge \#_{\perp}1 \quad (8)$$

and the velocity 1-form  $\tilde{V}$  and its Hodge dual are

$$\tilde{V} = du, \quad \star \tilde{V} = du \wedge \#_{\perp}1 \quad (9)$$

Taking the exterior derivative of the second Maxwell equation implies that the charge density is independent of  $\zeta$  and can thus be written  $\rho(r, \theta, u)$ . One may uniquely express  $F$  in terms of 0-forms  $\Phi(r, \theta, \zeta, u)$  and  $\Psi(r, \theta, \zeta, u)$ , and 1-forms  $\alpha_{\perp}(r, \theta, \zeta, u)$  and  $\beta_{\perp}(r, \theta, \zeta, u)$  which are independent of  $d\zeta$  and  $du$ :

$$F = \Phi d\zeta \wedge du + du \wedge \alpha_{\perp} + d\zeta \wedge \beta_{\perp} + \Psi \#_{\perp}1 \quad (10)$$

Furthermore, one may write [4]

$$\alpha_{\perp} = d_{\perp}A + \#_{\perp}d_{\perp}a, \quad \beta_{\perp} = d_{\perp}B + \#_{\perp}d_{\perp}b \quad (11)$$

for 0-forms  $A(r, \theta, \zeta, u)$ ,  $a(r, \theta, \zeta, u)$ ,  $B(r, \theta, \zeta, u)$  and  $b(r, \theta, \zeta, u)$  provided  $A$  and  $B$  vanish on the boundary  $\partial\mathcal{D}$ . This condition is compatible with the perfectly conducting boundary conditions that will be imposed on  $F$  below.

Without loss of generality, it proves expedient to re-write the form of  $F$  in terms of six new fields  $W$ ,  $X$ ,  $\mathcal{H}^B$ ,  $\mathcal{H}^b$ ,  $\mathcal{H}^{\Phi}$  and  $\mathcal{H}^{\varphi}$  that will facilitate our subsequent analysis;

$$\begin{aligned} A &= \partial_u W + \partial_{\zeta} W - \mathcal{H}^B, & B &= \mathcal{H}^B - \partial_{\zeta} W \\ \Phi &= \partial_u \mathcal{H}^{\Phi} + \partial_u \mathcal{H}^B + \partial_{\zeta} \mathcal{H}^B - 2\partial_{u\zeta}^2 W - \partial_{\zeta\zeta}^2 W \\ a &= \partial_u X, & b &= \partial_{\zeta} X - \mathcal{H}^{\varphi} \\ \Psi &= \partial_{\zeta} \mathcal{H}^{\varphi} + \partial_u \mathcal{H}^{\varphi} + \mathcal{H}^b - 2\partial_{u\zeta}^2 X - \partial_{\zeta\zeta}^2 X \end{aligned} \quad (12)$$

Thus, the Maxwell equations then reduce to the following relations:

$$\begin{aligned} \delta_{\perp} d_{\perp} \mathcal{H}^B &= 0 \\ d_{\perp} \mathcal{H}^b &= \#_{\perp} d_{\perp} (\partial_u \mathcal{H}^B), \quad d_{\perp} \mathcal{H}^{\varphi} = \#_{\perp} d_{\perp} \mathcal{H}^{\Phi} \\ \delta_{\perp} d_{\perp} W - 2\partial_{u\zeta}^2 W - \partial_{\zeta}^2 W \\ &\quad + \partial_u \mathcal{H}^{\Phi} + \partial_u \mathcal{H}^B + \partial_{\zeta} \mathcal{H}^B = P(r, \theta, u) \\ \delta_{\perp} d_{\perp} X - 2\partial_{u\zeta}^2 X - \partial_{\zeta}^2 X + \partial_{\zeta} \mathcal{H}^{\varphi} + \partial_u \mathcal{H}^{\varphi} + \mathcal{H}^b &= 0 \end{aligned} \quad (13)$$

where  $\partial_u P(r, \theta, u) = \frac{\rho(r, \theta, u)}{\epsilon_0}$ . The second equation in (13) implies the harmonic equations

$$\delta_{\perp} d_{\perp} \mathcal{H}^b = \delta_{\perp} d_{\perp} \mathcal{H}^{\varphi} = \delta_{\perp} d_{\perp} \mathcal{H}^{\Phi} = 0 \quad (14)$$

The waveguide wall is the spacelike hypersurface

$$f := r - R(\zeta) = 0 \quad (15)$$

for some smooth function  $R(\zeta)$ . We assume a perfectly conducting boundary condition for  $F$ :

$$df \wedge F = 0 \quad \text{at} \quad f = 0 \quad (16)$$

Equation (16) can be satisfied by setting

$$W = \partial_r X = 0, \quad \mathcal{H}^B = \partial_{\zeta} W, \quad \mathcal{H}^{\Phi} = -R'(\zeta) \frac{1}{r} \partial_{\theta} X \quad (17)$$

on the boundary  $f = 0$ .

## GRADUALLY TAPERING WAVEGUIDE

Consider first a regular cylindrical waveguide with constant radius  $R(\zeta) = R_0$ . As  $\partial_{\zeta} \rho = 0$ , the source and confining geometry are both symmetric with respect to translations in the  $\partial_{\zeta}$  direction. The simplest solution to the Maxwell system (13) with the boundary conditions (17) is then

$$X_0 = \mathcal{H}_0^b = \mathcal{H}_0^B = \mathcal{H}_0^{\Phi} = \mathcal{H}_0^{\varphi} = \partial_{\zeta} W_0 = 0 \quad (18)$$

$$\delta_{\perp} d_{\perp} W_0 = P(r, \theta, u) \quad (19)$$

with  $W_0 = 0$  on the boundary.

A waveguide is defined to be gradually tapering if

$$f := r - \check{R}(\epsilon\zeta) = 0 \quad (20)$$

where  $\epsilon$  is a small, dimensionless parameter. The fields will then vary slowly with  $\zeta$ . Introduce a ‘slow’ longitudinal coordinate

$$s = \epsilon\zeta \quad (21)$$

and rewrite all the potentials in terms of  $s$ , using the notation

$$\chi(r, \theta, \zeta, u) = \check{\chi}(r, \theta, s, u) \quad (22)$$

where  $\check{\chi} \in \{\check{W}, \check{X}, \check{\mathcal{H}}^B, \check{\mathcal{H}}^b, \check{\mathcal{H}}^{\Phi}, \check{\mathcal{H}}^{\varphi}\}$ . Express the potentials in the form of asymptotic series in  $\epsilon$ :

$$\check{\chi} = \sum_{n=0}^{\infty} \epsilon^n \check{\chi}_n \quad (23)$$

Note  $\partial_{\zeta} \chi = \epsilon \check{\chi}'$  (where, from now on, a prime denotes differentiation with respect to  $s$ ). The Maxwell equations (13) with boundary conditions (17) decouple to yield a hierarchical set of 2-dimensional Laplace and Poisson equations for every order  $n$ , and the boundary conditions on  $\check{\mathcal{H}}_n^B$  and  $\check{\mathcal{H}}_n^{\Phi}$  depend on  $(n-1)$ -order potentials. This leads to a straightforward procedure for calculating the potentials order-by-order. For  $n=0$ , the only non-zero potential is  $\check{W}_0$  which is a solution to  $\delta_{\perp} d_{\perp} W_0 = P(r, \theta, u)$  and vanishes at  $r = R(s)$ .

For every subsequent order of  $n$ :

1. Calculate the harmonic potential  $\check{\mathcal{H}}_n^B$  by solving the 2-dimensional Laplace equation

$$\delta_{\perp} d_{\perp} \check{\mathcal{H}}_n^B = 0 \quad (24)$$

subject to the boundary condition<sup>2</sup>

$$\check{\mathcal{H}}_n^B = \check{W}'_{n-1} \quad \text{at} \quad r = \check{R}(s) \quad (25)$$

2. Calculate  $\check{\mathcal{H}}_n^b$  from<sup>3</sup>

$$d_{\perp} \check{\mathcal{H}}_n^b = \partial_u \#_{\perp} d_{\perp} \check{\mathcal{H}}_n^B \quad (26)$$

3. Calculate the harmonic potential  $\check{\mathcal{H}}_n^{\Phi}$  by solving the 2-dimensional Laplace equation

$$\delta_{\perp} d_{\perp} \check{\mathcal{H}}_n^{\Phi} = 0 \quad (27)$$

subject to  $\check{\mathcal{H}}_n^{\Phi} = -\check{R}'(s) \frac{1}{r} \partial_{\theta} \check{X}_{n-1}$  at  $r = \check{R}(s)$

4. Calculate  $\check{\mathcal{H}}_n^{\varphi}$  from

$$d_{\perp} \check{\mathcal{H}}_n^{\varphi} = \#_{\perp} d_{\perp} \check{\mathcal{H}}_n^{\Phi} \quad (28)$$

5. Calculate the potential  $\check{W}_n$  by solving the 2-dimensional Poisson equation

$$\begin{aligned} \delta_{\perp} d_{\perp} \check{W}_n &= \check{W}''_{n-2} + 2\partial_u \check{W}'_{n-1} \\ &\quad - \partial_u \check{\mathcal{H}}_n^{\Phi} - \partial_u \check{\mathcal{H}}_n^B - \check{\mathcal{H}}_{n-1}^{B'} \end{aligned} \quad (29)$$

where  $\check{W}_n$  vanishes at  $r = \check{R}(s)$ .

6. Calculate the potential  $\check{X}_n$  by solving the 2-dimensional Poisson equation

$$\delta_{\perp} d_{\perp} \check{X}_n = \check{X}''_{n-2} + 2\partial_u \check{X}'_{n-1} - \check{\mathcal{H}}_n^b - \partial_u \check{\mathcal{H}}_n^{\varphi} - \check{\mathcal{H}}_{n-1}^{\varphi'} \quad (30)$$

with  $\partial_r \check{X}_n = 0$  at  $r = \check{R}(s)$

<sup>2</sup>Throughout this section, we are dealing with the *transverse* Laplacian  $\delta_{\perp} d_{\perp}$ . When considering the boundary conditions,  $s$  can thus be treated as a parameter.

<sup>3</sup>As  $\check{\mathcal{H}}_n^B$  is harmonic, the converse of Poincaré’s Lemma guarantees that a solution exists to (26).  $\check{\mathcal{H}}_n^b$  is thus defined up to arbitrary functions of  $s$  and  $u$ . These are subsequently constrained to zero by the boundary condition on  $\check{X}_n$ . By an analogous argument, a unique value for  $\check{\mathcal{H}}^{\varphi}$  can be obtained from  $\check{\mathcal{H}}^{\Phi}$  using (28).

## EXAMPLE

The method can be used to replicate and extend the longitudinal impedance<sup>4</sup> calculation in [2] for a harmonic Fourier component of a transverse delta-function beam offset from the central axis. In our notation, the source term and impedance formula are

$$\rho_\omega(r, \theta, u) = \lambda_\omega e^{i\omega u} \frac{1}{r} \delta(r - r_0) \delta(\theta) \quad (31)$$

$$Z_{\parallel}(\omega, r, \theta, u) = -Z_0 \frac{\varepsilon_0}{\lambda_\omega} \int_{-\infty}^{\infty} e^{-i\omega u} \Phi d\zeta \quad (32)$$

$$= -Z_0 \frac{\varepsilon_0}{\lambda_\omega} \frac{1}{\epsilon} \int_{-\infty}^{\infty} e^{-i\omega u} \check{\Phi} ds \quad (33)$$

where  $\lambda_\omega$  is the linear charge density,  $Z_0$  is the impedance of free space and  $\Phi$  is given by (12). First,  $\check{W}_0$  is obtained by solving  $\delta_{\perp} d_{\perp} \check{W}_0 = -\frac{i}{\omega} \rho_\omega(r, \theta, u)$  subject to Dirichlet boundary condition at  $r = \check{R}(s)$ . The solution is

$$\check{W}_0 = -\frac{i}{\omega} p(u) \left\{ \ln \left( \frac{r^2 r_0^2}{\check{R}(s)^2} + \check{R}(s)^2 - 2rr_0 \cos \theta \right) - \ln \left( r^2 + r_0^2 - 2rr_0 \cos \theta \right) \right\} \quad (34)$$

where  $p(u) := \frac{\lambda_\omega e^{i\omega u}}{4\pi\epsilon_0}$ . Furthermore,

$$\check{W}'_0 = -\frac{2i}{\omega} p(u) \frac{\check{R}'(s)}{\check{R}(s)} \left\{ 1 + 2 \sum_{m=1}^{\infty} \Upsilon_m(r, \theta, s) \right\} \quad (35)$$

where  $\Upsilon_m(r, \theta, s) := \left( \frac{r_0 r}{\check{R}(s)^2} \right)^m \cos m\theta$ . Evaluating the potentials according to the procedure in the previous section gives  $\check{\mathcal{H}}_1^B = W'_0$ ,  $\check{\mathcal{H}}_1^\Phi = \check{\mathcal{H}}_1^\varphi = 0$  and

$$\check{\mathcal{H}}_1^b = 4p(u) \frac{\check{R}'(s)}{\check{R}(s)} \sum_{m=1}^{\infty} \left( \frac{r_0 r}{\check{R}(s)^2} \right)^m \sin m\theta \quad (36)$$

$$\check{W}_1 = \frac{p(u)}{2} \frac{\check{R}'(s)}{\check{R}(s)} (\check{R}(s)^2 - r^2) \left[ 1 + \sum_{m=1}^{\infty} \frac{2\Upsilon_m(r, \theta, s)}{1+m} \right] \quad (37)$$

$$\check{X}_1 = p(u) \frac{\check{R}'(s)}{\check{R}(s)} \sum_{m=1}^{\infty} \frac{1}{1+m} \left( \frac{r_0 r}{\check{R}(s)^2} \right)^m \times \left( r^2 - \frac{m+2}{m} \check{R}(s)^2 \right) \sin m\theta \quad (38)$$

$$\check{\mathcal{H}}_2^B = p(u) \check{R}'(s)^2 \left[ 1 + \sum_{m=1}^{\infty} \frac{2\Upsilon_m(r, \theta, s)}{1+m} \right] \quad (39)$$

$$\check{\mathcal{H}}_2^\Phi = 2p(u) \check{R}'(s)^2 \sum_{m=1}^{\infty} \frac{\Upsilon_m(r, \theta, s)}{1+m} \quad (40)$$

As can be seen from the equation for  $\Phi$  in (12),  $\check{\mathcal{H}}_2^b$ ,  $\check{\mathcal{H}}_2^\varphi$ ,  $\check{W}_2$  and  $\check{X}_2$  are not required in order to evaluate the

impedance to second order. The longitudinal electric field at this approximation is

$$\check{\Phi} = p(u) \left\{ 2\epsilon \frac{\check{R}'(s)}{\check{R}(s)} \left[ 1 + 2 \sum_{m=1}^{\infty} \Upsilon_m(r, \theta, s) \right] + i\omega\epsilon^2 \left[ \left( \frac{\check{R}'(s)}{\check{R}(s)} (r^2 - \check{R}(s)^2) \left[ 1 + \sum_{m=1}^{\infty} \frac{2\Upsilon_m(r, \theta, s)}{1+m} \right] \right)' + \check{R}'(s)^2 \left( 1 + 4 \sum_{m=1}^{\infty} \frac{\Upsilon_m(r, \theta, s)}{1+m} \right) \right] \right\} \quad (41)$$

The longitudinal impedance follows from (33). If the waveguide approaches constant radii  $R_1$  as  $s \rightarrow -\infty$  and  $R_2$  as  $s \rightarrow \infty$ , then  $R'(s) = 0$  at  $s = \pm\infty$  and the second line of (41) will not contribute to the integral. Thus, to this approximation,

$$Z_{\parallel} = Z_0 \frac{\varepsilon_0}{4\pi\lambda_\omega} \left\{ 2 \ln \frac{R_1}{R_2} - i\omega\epsilon \int_{-\infty}^{\infty} \check{R}'(s)^2 ds + \sum_{m=1}^{\infty} \left( \Upsilon_m \Big|_{R(s)=R_1}^{R(s)=R_2} - \frac{4i\omega\epsilon}{1+m} \int_{-\infty}^{\infty} \Upsilon_m \check{R}'(s)^2 ds \right) \right\} \quad (42)$$

After changing variable from  $s$  to  $\zeta$  and truncating the series at  $m = 1$ , the second-order impedance (42) is identical to the tapered cylinder result in [2]. Evaluating  $\check{W}_2$  and  $\check{X}_2$  and repeating the procedure of the previous section for  $n = 3, 4, \dots$  yields higher order correction terms. The third order correction turns out to be zero for an asymptotically cylindrical pipe. The fourth order correction is

$$Z_{\parallel 4} = \frac{Z_0 \varepsilon_0}{4\pi\lambda_\omega} i\omega\epsilon^3 \int_{-\infty}^{\infty} (\Lambda_1 \check{R}'(s)^4 + \Lambda_2 \check{R}''(s)^2 \check{R}(s)^2) ds \quad (43)$$

where

$$\Lambda_1 = \frac{5}{24} + \sum_{m=1}^{\infty} \frac{\Upsilon_m \kappa_{1m}}{3} (2m^2 + 6m + 1 - \omega^2 (4m - 3) \kappa_{2m} \check{R}(s)^2)$$

$$\Lambda_2 = \frac{3}{24} - \frac{\omega^2}{12} \check{R}(s)^2 + \sum_{m=1}^{\infty} \Upsilon_m \kappa_{1m} (1 - \omega^2 \kappa_{2m} \check{R}(s)^2)$$

$$\kappa_{1m} = \frac{2}{m(m+1)(m+2)}, \kappa_{2m} = \frac{3m^2 + 8m + 6}{m(m+1)^2(m+3)}$$

while the fifth order contribution is zero.

## REFERENCES

- [1] Stupakov G V Part. Accel. **56**, 83 (1996)
- [2] Stupakov G V, Phys. Rev. ST Accel. Beams **8** 094401 (2007)
- [3] Tucker R W, Theoretical and Applied Mechanics, 34 (1):1-49 (2007)
- [4] Abraham R, Marsden J E, Ratiu T *Manifolds, Tensor Analysis and Applications* (New York: Springer-Verlag, 1988)
- [5] Panofsky W K H, Wenzel W Rev. Sci. Instrum. **27** 967 (1956)

<sup>4</sup>Transverse impedance can be obtained from the Panofsky-Wenzel relation [5].