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THE RAYTRACING OF A FOCUSSING MIRROR FOR PX AND SSP STATIONS ON STORAGE RING "SIBERIA-2" (MOSCOW, USSR)

by

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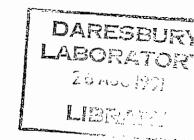
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The Raytracing of a Focussing Mirror for PX and SSP Stations on Storage Ring "Siberia - 2" (Moscow USSR).

by V. I. Raiko[†] and A. W Thompson².

Abstract.

This report describes the use of the MAXRAY raytracing package /1,2/ in assessing the design of a focussing mirror for the Protein Crystallography (PX) and Solid State Physic (SSP) stations due to be constructed on the storage ring "SIBERIA - 2" in Moscow. Focussing optics are required for PX because of the large discrepancy in size of the diverging synchrotron radiation beam and a protein crystal sample (typically 0.3 x 0.3 x 0.3 mm³). The efficiency of X - ray collection is investigated as a function of grazing angle, magnification and misalignment error for both toroidal and ellipsoidal mirror forms.

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1. Introduction.

The storage ring "SIBERIA-2" is under construction at the Moscow Kurchatov Institute of Atomic Energy /3/. The main parameters of the storage ring are presented in Table 1. The Institute of Molecular Genetics (USSR Academy of Sciences) are planning several biological stations including Protein Crystallography (PX) - a full list of the planned workstations is given in Table 2. The schematic layout of the biological beamline is given in Fig 1, and includes an experiment at 29.5m from the tangent point of D24 - 2 for PX, and one at 25.5m from the tangent point for solid state physics (SSP) investigations. The raytracing investigation was required in order to determine whether these two stations could use the same focussing mirror, and to evaluate the aberrations associated with the two focussing positions (1.3:1 and 2:1). The effect of mirror misalignments was also investigated in order to simulate incorrect mirror mounting and positioning.

2. Raytracing.

The MAXRAY package was developed at Uppsala University, and has already been used at Daresbury in the study of a mirror for a PX station /4/. Each optical element is represented by a subroutine, with rays from a simulated synchrotron source distribution being traced through each element to the image plane. The output of the program therefore consists of a predicted two dimensional intensity distribution which can be integrated over an area of interest (for example, the size of a typical X - ray collimator) in order to estimate the overall efficiency of focussing. The drawback of the ray tracing approach is that the images so produced represent those from a perfectly figured mirror, unaffected by the heat load of the X - rays incident on it, and with zero surface roughness. Prior to any raytracing analysis it is important to take into account the above parameters and their likely impact on the quality of focus and reflectivity.

3. Results.

The following questions were addressed:-

- a) What is the optimum length of mirror taking into account collection efficiency, beam acceptance and reflectivity, cost and difficulty of fabrication?
- b) Would it be more efficient to use a small ellipsoid than a large toroid?
- c) Is it possible to share a mirror between the two stations described above either by using a

fixed figure mirror and changing the grazing angle, or by refocussing a toroidal mirror?

d) What is the optimum magnification to use, and how quickly does aberration begin to dominate the image when working away from this position?

The flux from the storage ring at various energies was calculated using the program due to Laundy /5/ for a stored beam of 100 mA and integrated over several vertical beam apertures corresponding to many possible combinations of mirror length and grazing angle. These fluxes were than multiplied by the calculated reflectivity of a Pt mirror with a typical (good!) surface roughness of 10Å rms. The results of these calculations are shown for various mirror lengths and the preferred grazing angle of 3 mrad in Fig 2. It can be seen that there is a decreasing return in going for longer and longer mirrors when the escalating price and difficulty of fabrication is taken into account. It was therefore deemed unnecessary to increase the mirror length beyond 60 - 80 cm.

The 3 mrad grazing angle was selected as the largest possible grazing angle (for a Pt coated mirror) to give the required wavelength spread (0.5Å - 2.0Å) for Laue crystallography.

The efficiency of collection of rays from the mirror was calculated by summing the rays falling within in a user selected box centred around the peak intensity. The number of rays falling within this area is expressed as a percentage of the total number of rays striking the mirror, and was calculated for square boxes with 0.3mm, 0.5mm and 0.7mm edges. This forms a sensible estimate only if a sufficiently large total number of rays are traced (thus overcoming any non-randomness due to the "seed" used to generate the starting point of the ray in the computer code).

A number of raytraces of the effects of different mirror parameters were carried out in order to model the sensitivity of various mirror misalignments.

In order to share a mirror between the SSP and PX modes of beamline D24 - 3 (distances 9m and 13m from the mirror position), the curvatures of two types of mirror (toroid and ellipsoid) were optimised for a point in between the two stations (11m) and the two systems traced at various grazing angles. The results of the calculations are presented in Table 3. The better focussing at 9m (about 50% of optimum value) is achieved for 3.4 mrad graze angle, and at 13m for 2.7 mrad - Figs 3 and 4 show the corresponding focal spots.

4. Discussion.

The raytracing for the ellipsoidal mirror shows the expected very high quality of focus. These mirrors, however, are extremely difficult to fabricate, particularly if a large (60 - 80 cm) mirror is required. Therefore, for focussing ratios close to 1:1, a toroidal mirror is used to approximate the shape of an ellipsoid.

Fig 5 shows the calculated focal spot produced by an ideal toroid for the magnification

required to focus the beam at the PX station (M = 0.78). This gives approximately 30% less intensity in a 0.3mm square box than the M=I case (Fig 6). Moreover, the efficiency of the focus of the real mirror will be critically dependent on the figure accuracy of the mirror, and (in particular) on the slope error. This is the "flatness" of the surface in the long direction of the mirror, and effectively makes the mirror appear as several mirrors at slightly different grazing angles. When the slope error is around 2 are seconds, the vertical focus is doubled in size. These slope errors are simulated in Fig 7 by varying the graze angle by +10 and -10 are seconds. The overall image obtained with a 20 second slope error would be the superposition of these images.

The effect on the focussing properties of changing the sagittal radius from the optimum is illustrated in Fig 8. Figs 9 and 10 show the very critical variation of yaw angle (the rotation of the mirror around an axis perpendicular to its surface) with the toroid efficiency. It is important that corrections of smaller than 0.05 mrad over the length of the mirror can be made.

An illustration of the effect of a mirror translation about the optimum position is shown in Fig 11. The effect of a mirror rotation around a longitudinal axis (roll) is given in Fig 12. The variation in the efficiency of a toroid optimised to focus at an image distance of 13m is shown in Fig 13.

It should be pointed out that arguments about slope error, figure and off axis source still apply to the ellipsoidal mirror where there are similar difficulties in aligning the mirror. The opportunity of refocussing the mirror for different image distances is also lost.

List of Figures.

- Layout of the proposed biological stations on SIBERIA 2.
- The calculated intensity x reflectivity for SIBERIA 2, with 100 mA of stored beam incident on various lengths of Pt coated (plane) mirror.
- 3. The focal spot calculated at a distance of 9m from the toroidal mirror position.
- The focal spot calculated at a distance of 13m.
- 5 a. The focal spot for the ideal toroid optimised for an image distance of 13m.
- b. As 5a, but the information is now presented as a surface plot.
- c. As 5a, but the information is now presented as a contour map.
- 6. Plot of toroid efficiency vs magnification.
- 7 a. The effect on the focus of mis-setting the graze angle to 3.05 mrad.
- b. The effect on the focus of mis-setting the graze angle to 2.95 mrad.
- 8 a. The effect on the focus of an incorrectly figured sagittal curvature (optimum -1.1mm).
- b. The effect on the focus of an incorrectly figured sagittal curvature (optimum +0.9mm).
- Variation of yaw angle with toroid efficiency.
- 10. The effect on the focus of a 0.1 mrad yaw error.
- 11. The effect of moving the mirror 1.5 mm above the beam axis.
- 12. The effect of a 15 mrad roll error.
- The variation of efficiency with image distance, for an optimum image distance of 13m.

Table 1.

Main Parameters for the SIBERIA - 2 Storage Ring.

Electron Energy	2.5	GeV
Beam Current		
single bunch	100	mA
multi bunch	300	mA
Emittance		
horizontal	76.5	rad. nm
vertical	0.76 *	rad. nm
Bending Magnets		
Magnetic Field	1.7	Т
Bending Radius	4.9054	m
SR Critical Energy	7.1	keV

^{*} Preliminary data.

The Biological Experiments Proposed for SIBERIA - 2.

BEAM LINE	D24 - 1+	D24 - 2 ⁺	D24 - 3 W1 - 1*		W1 - 1
SOURCE	BENDING	BENDING	BENDING	WIGGLER	WIGGLER
	MAGNET	MAGNET	MAGNET		
EXPERIMENT	ISOMORPHOUS	POLYCHROMATIC MAD, EXA		LAUE	TIME
	REPLACEMENT	X - RAY DIFFRAC-			RESOLVED
		TION			LAUE
WAVELENGTH (Å)	1	0.5 - 3.0	0.5 - 3.0	0.2 - 3.0	0.2 - 3.0
<u>δλ</u>	10-3	10 ⁻² - 10 ⁻³	<10⁴	10.1	10-1
EXPECTED FOCAL SPOT SIZE [MM X MM]	1 x 1	1 x 1	0.3 x 0.3	UNFOCUSS ED	UNFOCUSS ED
MONOCHROMATOR	BENT TRIANGLE	BENT TRIANGLE	TWO CRYS-	n/a	n/a
MIRROR	CYLINDRICAL	CYLINDRICAL	TOROIDAL	n/a	n/a
DETECTOR	MWPC	FILM	MWPC	FILM	FILM

Note that * and * represent shared stations.

Table 2.

Table 3.

Efficiency of Toroid vs Ellipsoid

The efficiency (as a percentage of total number of rays traced) of a simulated toroid and ellipsoid are given for image collection at 9m (SSP station) and 13m (PX station) from the mirror for beam line D24 - 3. The figure of the two mirrors is optimised for a focus between the two stations i.e. at 11m from the mirror. The grazing angle of the two mirrors is adjusted to achieve better focussing, but the curvatures of the surfaces remain fixed. The optimum focus (at 11m) of the two mirrors is also given.

TOROID	Graze Angle [mrad]	0.3 mm collimator	0.5 mm collimator	0.7 mm collimator	Distance [m]
	2.6	6.5	12.8	19.6	13m
	2.7	16.8	35,2	48.5	13m
	2.8	9.6	26.7	50.1	13m
	3.3	10.6	25.9	44.1	9m
	3.4	22.8	43.2	67.4	9m
	3.5	9.9	20.7	33.2	9m
OPTIMUM	3.0	44	58.2	69.3	11m
ELLIPSOID	2.6	5.1	11,1	18.8	13m
	2.7	24.6	49.1	68	13m
	2.8	9.3	15	25.7	13m
	3.3	14.3	27.2	48.5	9m
	3.4	35.3	62.4	90.4	9m
	3.5	8.7	21	36.3	9m
OPTIMUM	3.0	88.9	99.5	100	11m

References.

- [1] S. Svensson and R. Nyholm. Uppsala University Institute of Physics Report UUIP 1139 (1985).
- [2] R. C. Brammer. Raytracing with MAXRAY and the Design of PX Station 9.5. Daresbury Lab. Technical Memorandum DL/SCI/TM56E (1987).
- [3] S. D. Fanchenko. Synchrotron Radiation News 3 (1990) 6 9.
- [4] R. C. Brammer et Al. NIM <u>A271</u> (1988) 678 687.
- [5] D. Laundy et Al. DL/SCI/P683E Submitted to NIM March 1990.

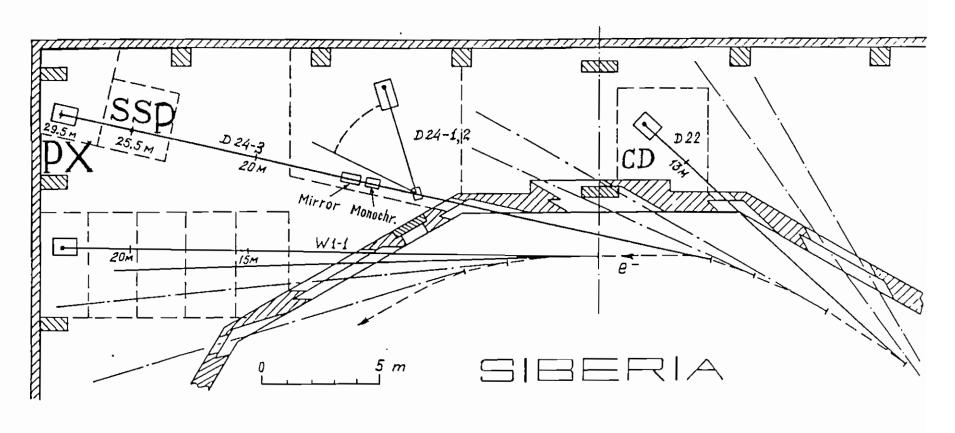


FIG-1

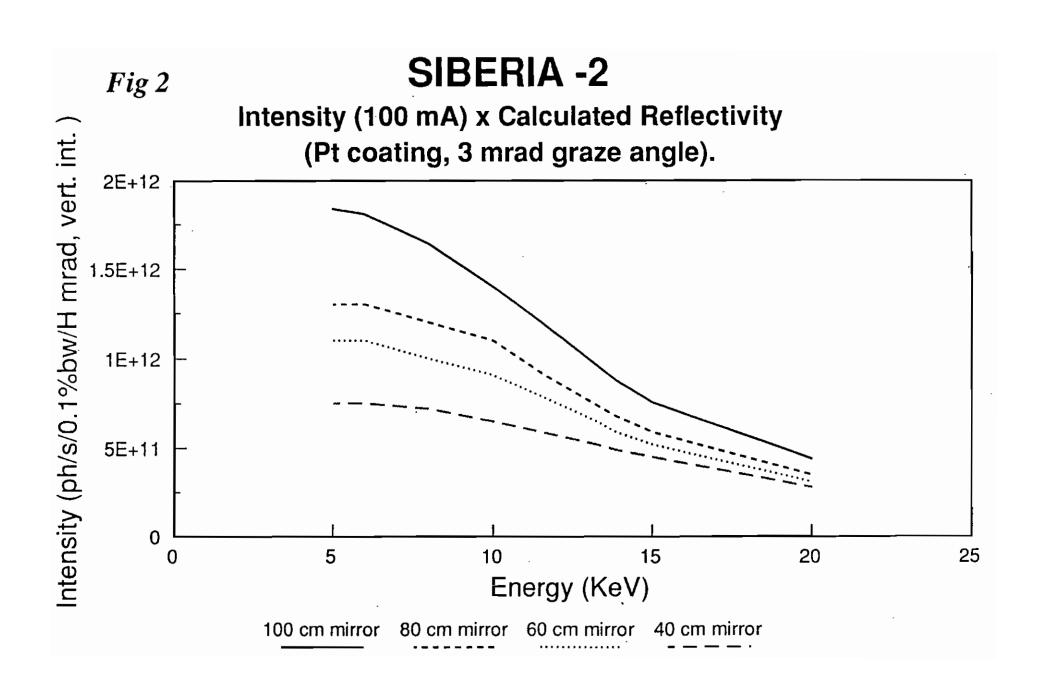
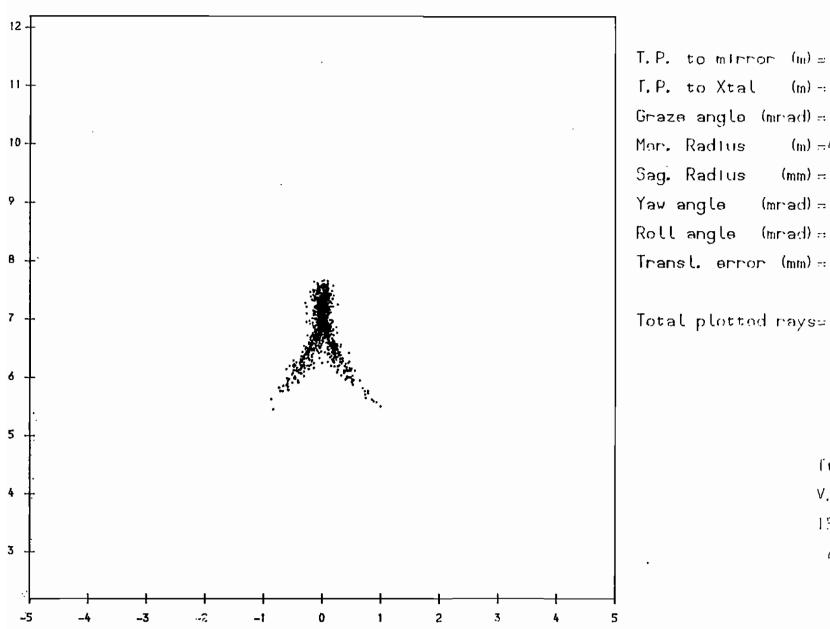
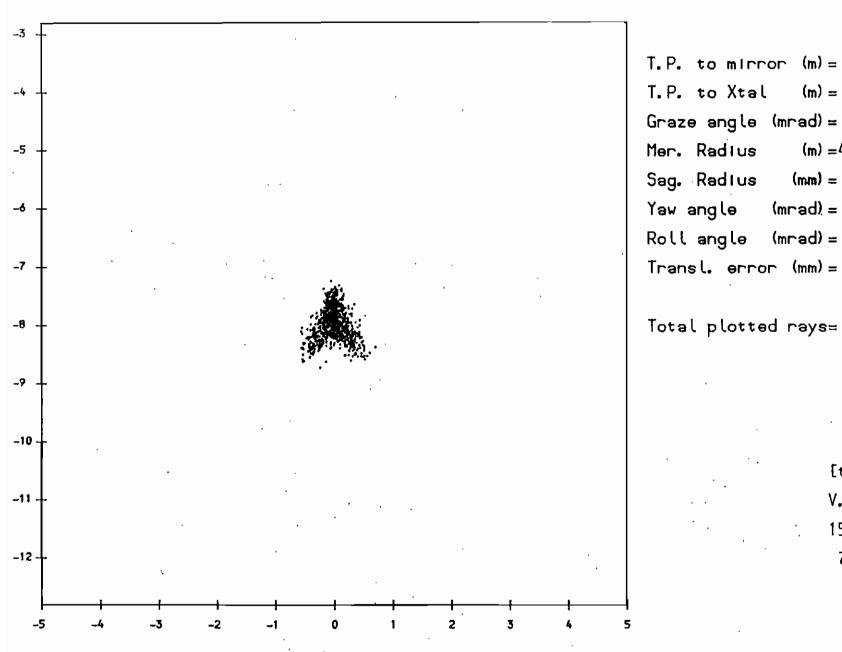


Fig 3



T.P. to mirror (m) = 16.500T.P. to Xtal (m) -: 25.500 Graze angle (mrad) = 3.400 Mor. Radius (m) = 4400,000Sag. Radius (mm) = 39.600Yaw angle (mrad) = 0.000 Roll angle (mrad) == 0.000 Transt. error (mm) == 0.000

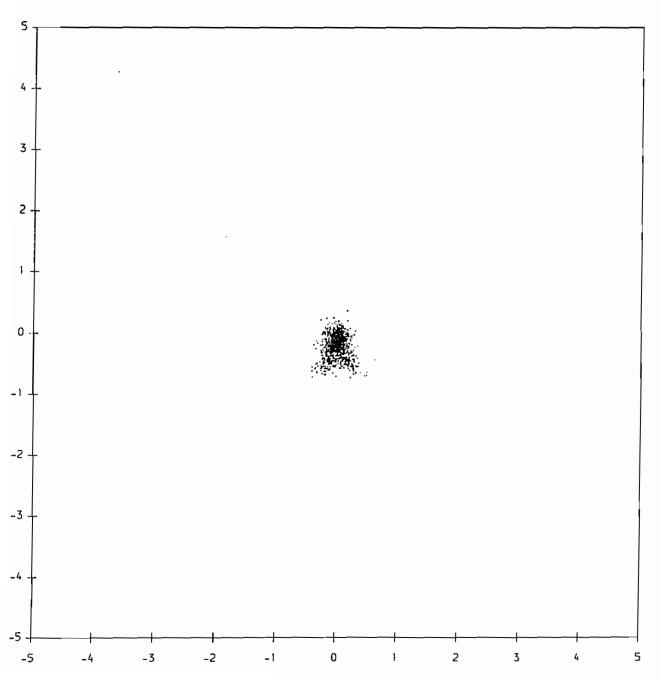
> fil. plotitorgit V. Rajko 15,35,46 7/MAR/90



T.P. to mirror (m) = 16.500T.P. to Xtal (m) = 29.500Graze angle (mrad) = 2.700 Mer. Radius (m) =4400.000 Sag. Radius (mm) = 39.600Yaw angle (mrad) = 0.000 Roll angle (mrad) = 0.000 Transt. error (mm) = 0.000

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Fig 5a

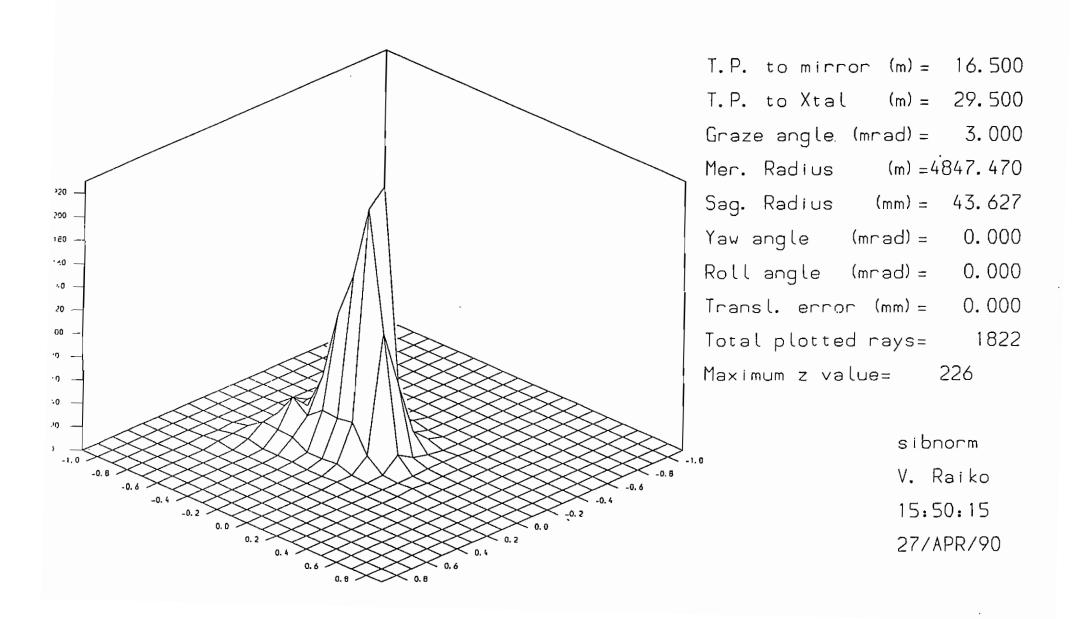


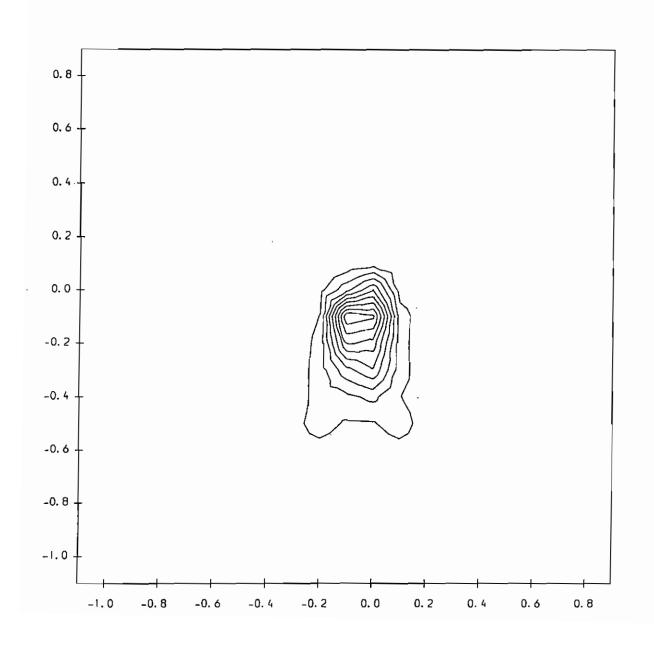
T.P. to mirror (m) = 16.500
T.P. to Xtal (m) = 29.500
Graze angle (mrad) = 3.000
Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 43.627
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000
Transl. error (mm) = 0.000

Total plotted rays= 1822

sibnorm V. Rajko 15:45:44

27/APR/90





T.P. to mirror (m) = 16.500
T.P. to Xtal (m) = 29.500
Graze angle (mrad) = 3.000
Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 43.627
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000
Transl. error (mm) = 0.000
Total plotted rays = 1822
Maximum z value = 226

sibnorm

V. Raiko

15:43:09

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SIBERIA - 2

Toroid Efficiency vs Magnification

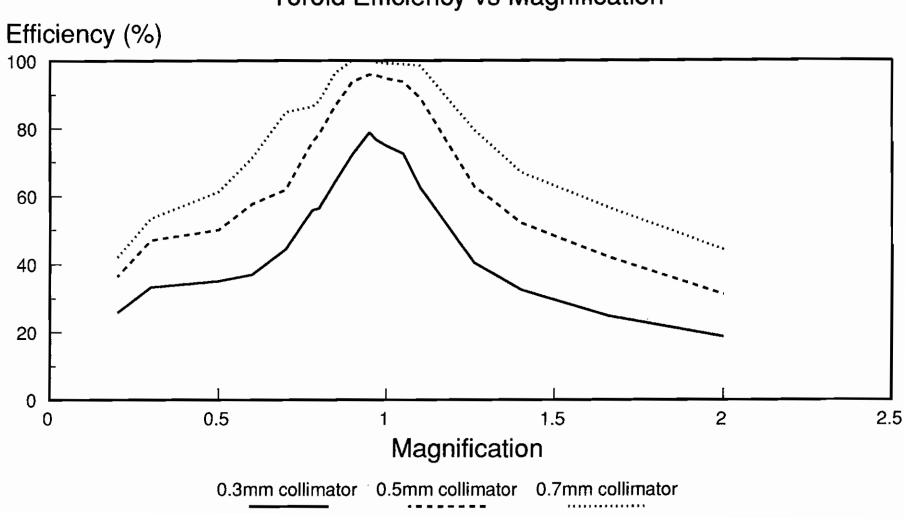
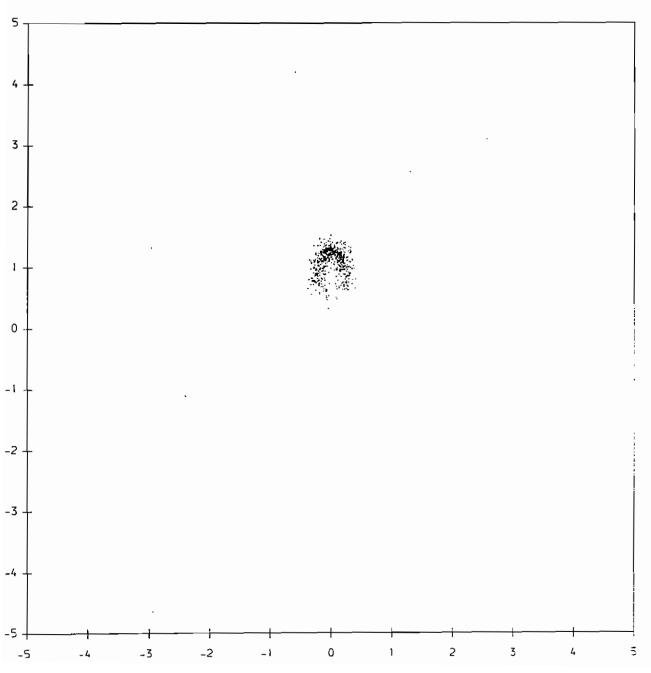


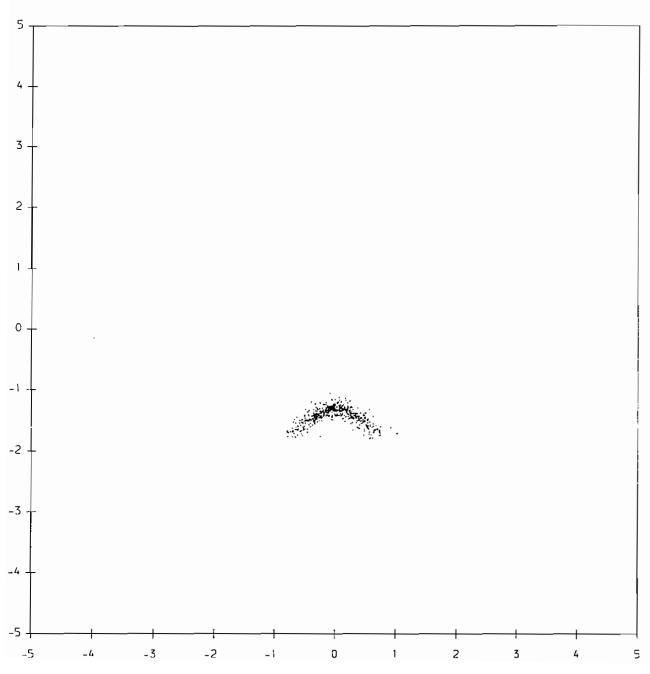
Fig 7 a



T.P. to mirror (m) = 16.500
T.P. to Xtal (m) = 29.500
Graze angle (mrad) = 3.050
Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 43.727
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000
Transl. error (mm) = 0.000

Total plotted rays= 570

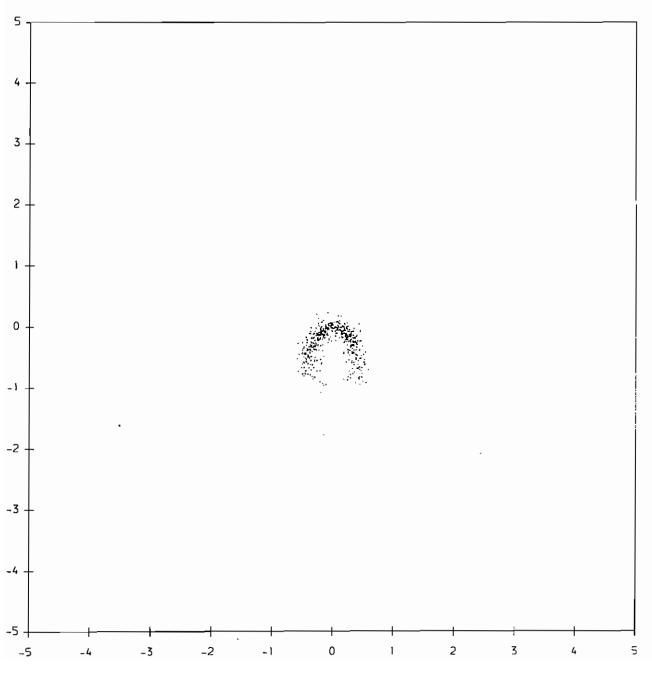
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Ron Brammer
17:59:50
27/FEB/90



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T.P. to Xtal (m) = 29.500
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Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 43.727
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000
Transl. error (mm) = 0.000

Total plotted rays=

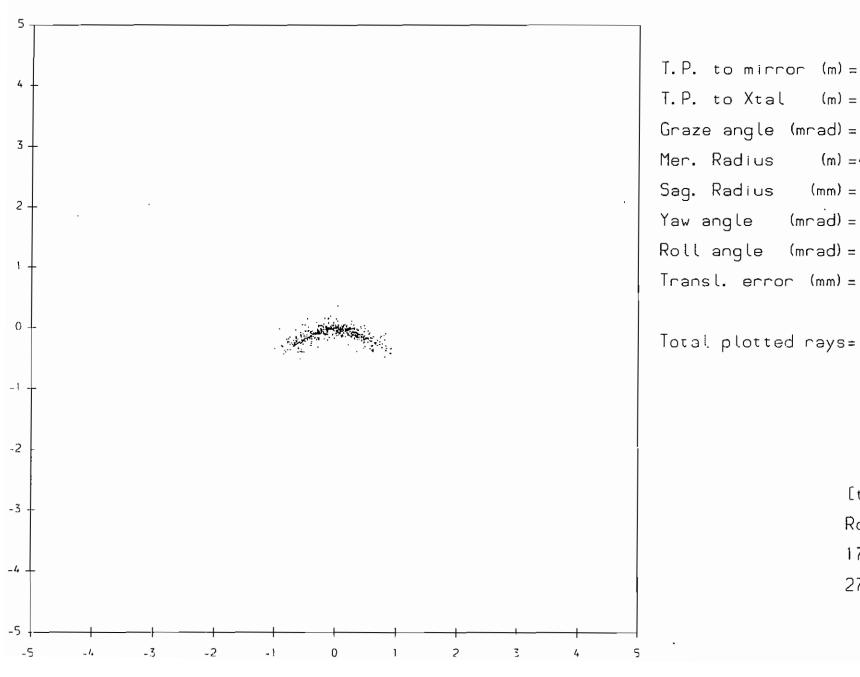
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Ron Brammer
18:00:55 .
27/FEB/90



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T.P. to Xtal (m) = 29.500
Graze angle (mrad) = 3.000
Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 42.627
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000
Transl. error (mm) = 0.000

Total plotted rays=

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Ron Brammer
17:33:37
27/FEB/90



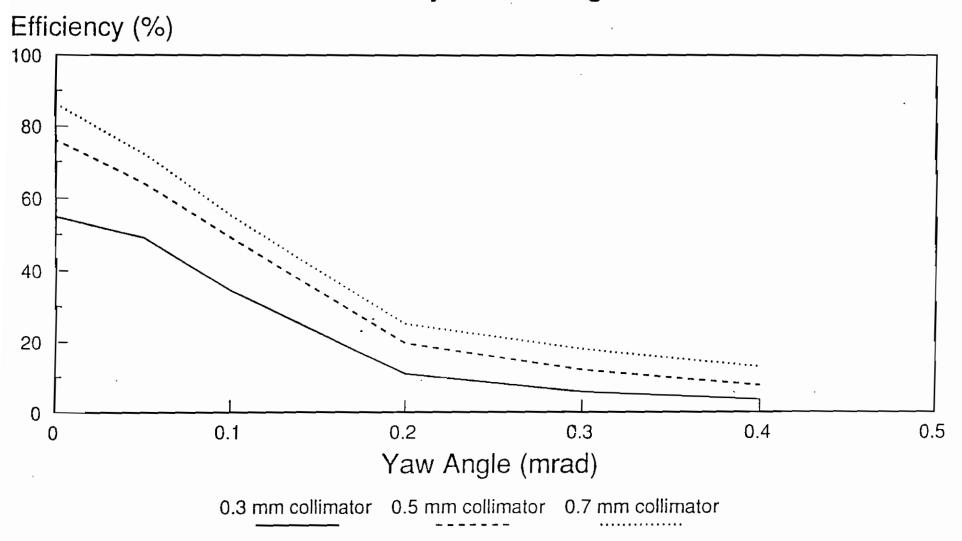
T.P. to mirror (m) = 16.500T.P. to Xtal (m) = 29.500Graze angle (mrad) = 3.000 Mer. Radius (m) = 4847.470Sag. Radius (mm) = 44.627Yaw angle (mrad) = 0.000 Roll angle (mrad) = 0.000 Transl. error (mm) = 0.000

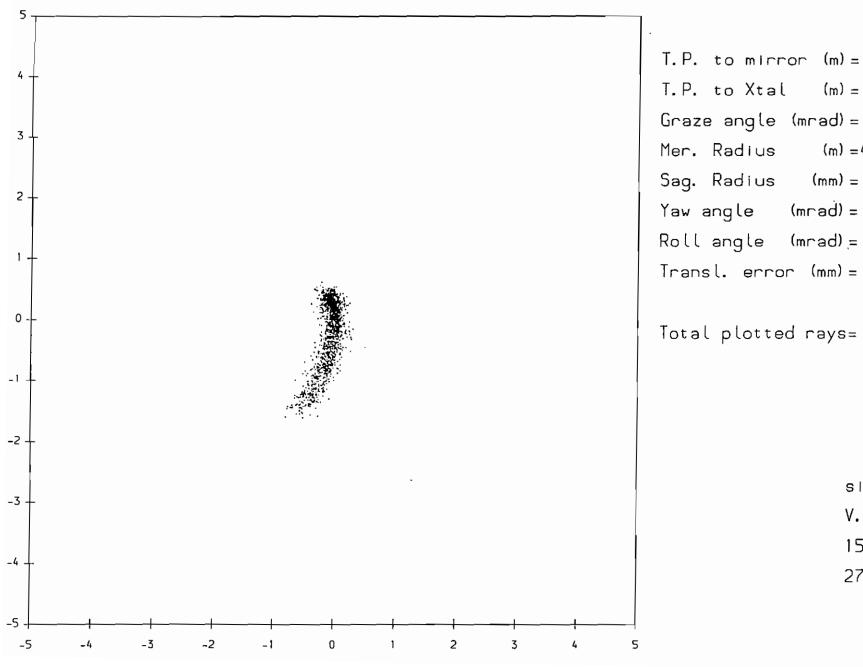
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SIBERIA -2

Fig 9

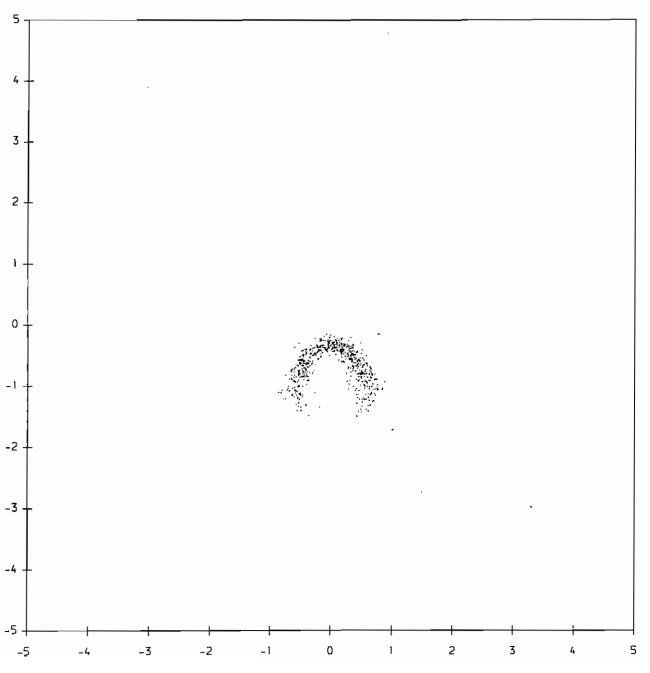
Efficiency vs Yaw Angle





T.P. to mirror (m) = 16.500(m) = 29.500T.P. to Xtal Graze angle (mrad) = 3.000 Mer. Radius (m) = 4847.470Sag. Radius (mm) = 43.627Yaw angle (mrad) = 0.100 Roll angle (mrad) = 0.000 0.000 Transl. error (mm) =

> sibyaw V. Rajko 15:46:54 27/APR/90



T.P. to mirror (m) = 16.500
T.P. to Xtal (m) = 29.500
Graze angle (mrad) = 3.000
Mer. Radius (m) = 4847.470
Sag. Radius (mm) = 43.627
Yaw angle (mrad) = 0.000
Roll angle (mrad) = 0.000

Total plotted rays= 605

Transl. error (mm) = 1.500

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V. Rajko
17:03:51
6/MAR/90

```
125
0.000
        = (mm) nonne .lenenT
                 Boll angle
        = (beam)
12.000
                 algne weY
000.00
        = (benm)
        = (ww)
               Sag. Radius
7<u>2</u>2 .27
025 °2585= (W)
             Mer. Radius
        = (benm) algne asend
3,000
29, 500
        = (m) JetX of .T
T. P. to mirror (m) = 16,500
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